



HIRENASD Analysis Using MSC NASTRAN OpenFSI and CFD++

**1st Aeroelastic Prediction Workshop
Honolulu, Hawaii
April 21-22**

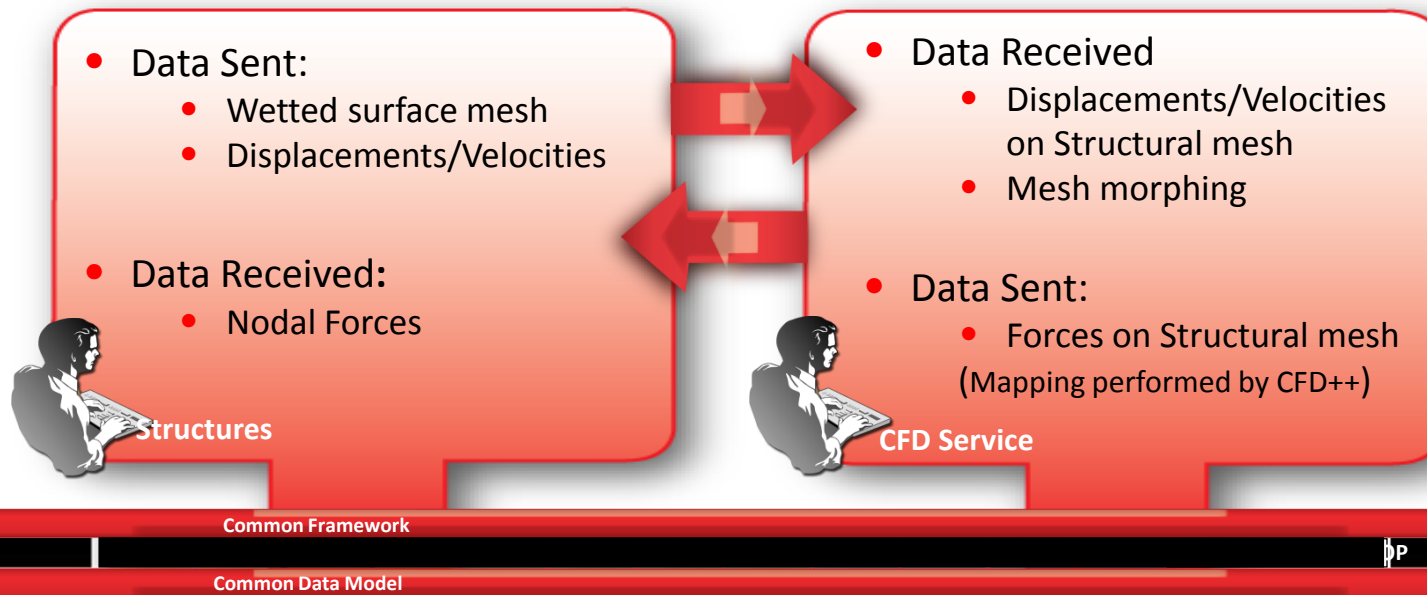
**Beerinder Singh (Metacomp)
Jack Castro (MSC)**

Agenda

- **Solution Approach**
- **Setup**
- **Results Discussion**
- **Runtimes**
- **Lesson's Learned/Next Steps**

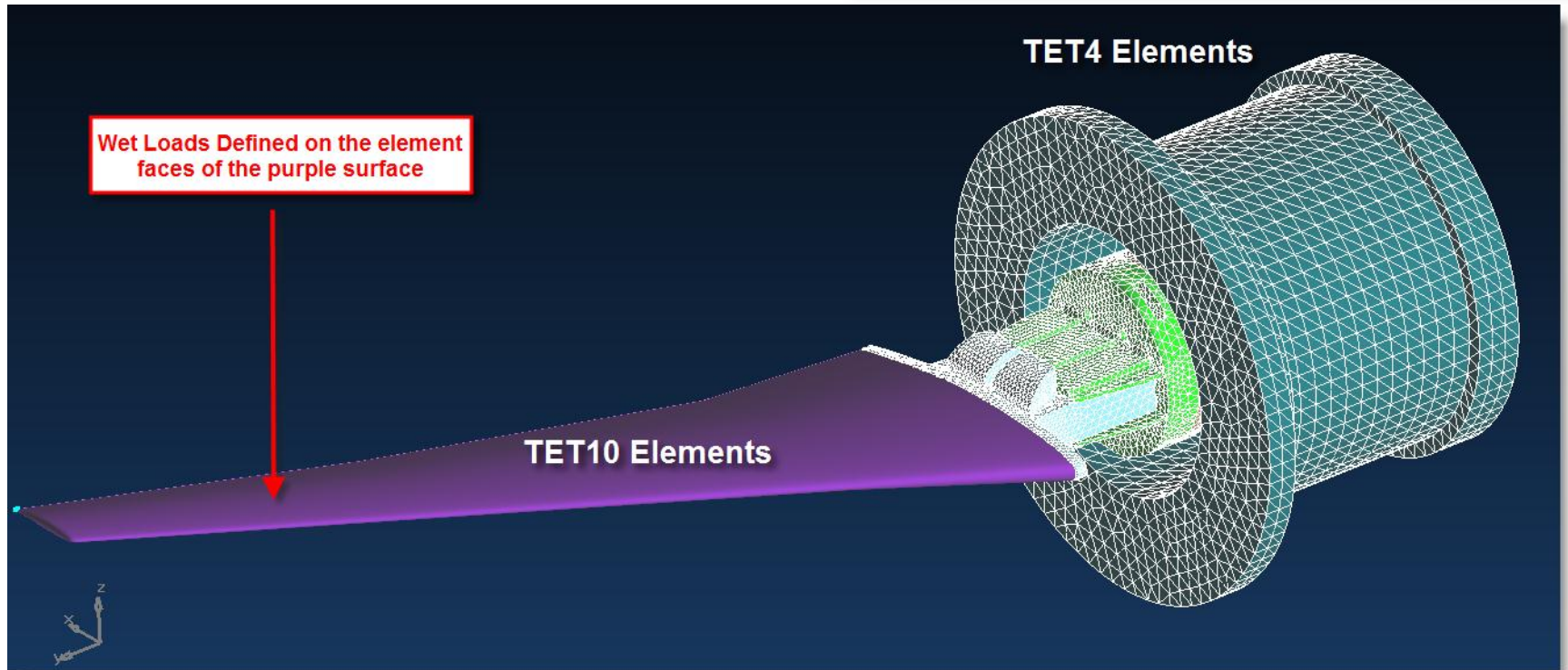
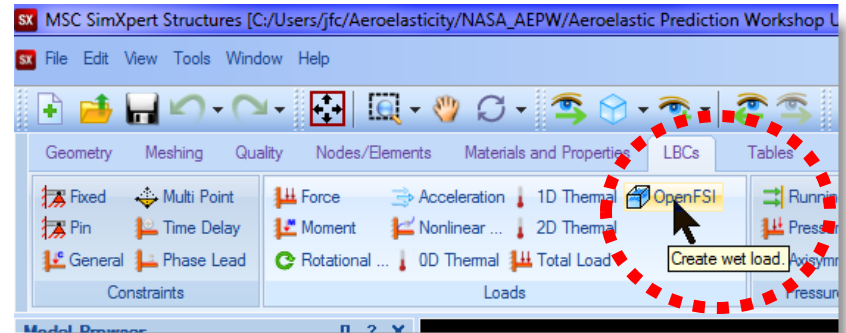
Solution Approach

- **MSC Nastran OpenFSI Service**
 - Co-simulation with CFD++
 - Structural FSI -- Forces and Displacements/Velocities
 - Static/Steady or Transient/Unsteady linear/nonlinear solutions
 - Available in MSC Nastran SOL 400



MSC Nastran Setup

- SOLution 400
- Define “WetLoad”
 - Wetload → WetSurf → WetElm



Tet4/Tet10 Combined Model Mode Comparison

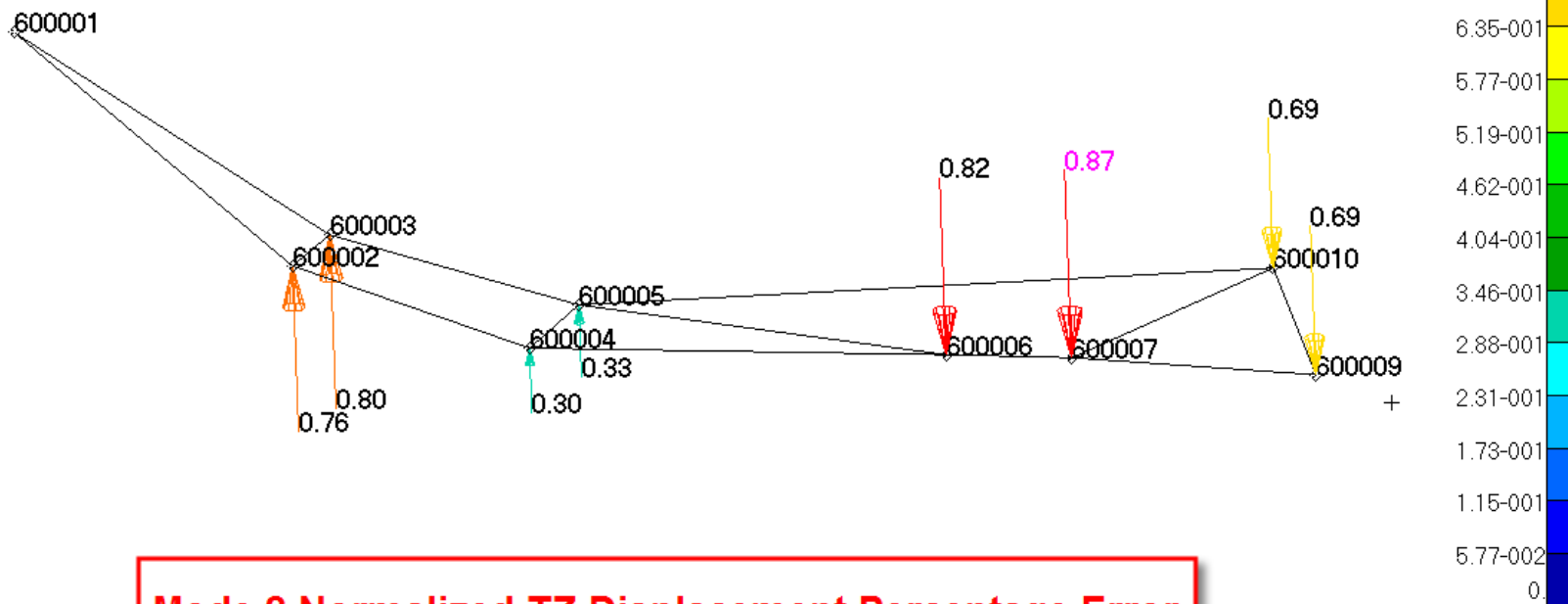
| Mode | All Tet10 | Tet4/Tet10 Wing | Experiment |
|------|-----------|-----------------|------------|
| 1B | 25.550 | 25.560 | 26.015 |
| 2B | 80.245 | 80.931 | 78.635 |
| 1FA | 106.193 | 110.994 | |
| 3B | 160.349 | 165.228 | 166.250 |
| 4B | 241.995 | 250.552 | 245.002 |
| 1T | 271.884 | 272.926 | 265.885 |

Tet4/Tet10 Combined Model Mode Comparison

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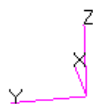
Vector: Percent_AB, Subcase 35, Eigenvectors, Translational, , (NON-LAYERED)

Deform: Untitled.SC1, A1:Mode 2 : Freq. = 80.245, Eigenvectors, Translational, , (NON-LAYERED)



**Mode 2 Normalized TZ Displacement Percentage Error
(Relative to all Tet10 Model)**

default_Vector :
Max 0.87 @Nd 600007
Min 0.00 @Nd 600001



MSC Nastran Setup

CONNECT SERVICE FSISRV1 'metacfd.openFSI'

```
SOL 400
CEND
SPC = 1
smethod=element
set 1 = 600001 thru 600007, 600009,600010
SUBCASE 1
  DLOAD = 1001
  ANALYSIS = NLTRAN
  NLSTEP = 1
  IC=101
BEGIN BULK
```

FSICTRL FSISRV1 EXPLICIT 1

```
$ damping
param,g,0.2
param,w3,495.7 $ 2*pi*78.9
$
$ 78.9 hz = period of 0.01267
$ 5 periods = .0634 sec
$ 500 steps
NLSTEP 1 .0634
      general 25 2 0
      fixed 500
```

```
INCLUDE 'tet4_mc.dat' $ structural model
INCLUDE 'hirenasd_TIC_Case159-nospc.dat' $ transient initial conditions
```

```
DLOAD 1001 1. 1. 21
$ wet load is TLOAD1,21
TLOAD1 21 2 3
$ the table below will apply all the wet load at time zero
TABLED1 3
      0.0 1. 10000. 1. endt
```

\$ OPENFSI LOADING

\$!

| | | |
|---------|---|-----------|
| WETLOAD | 2 | 2 FSISRV1 |
|---------|---|-----------|

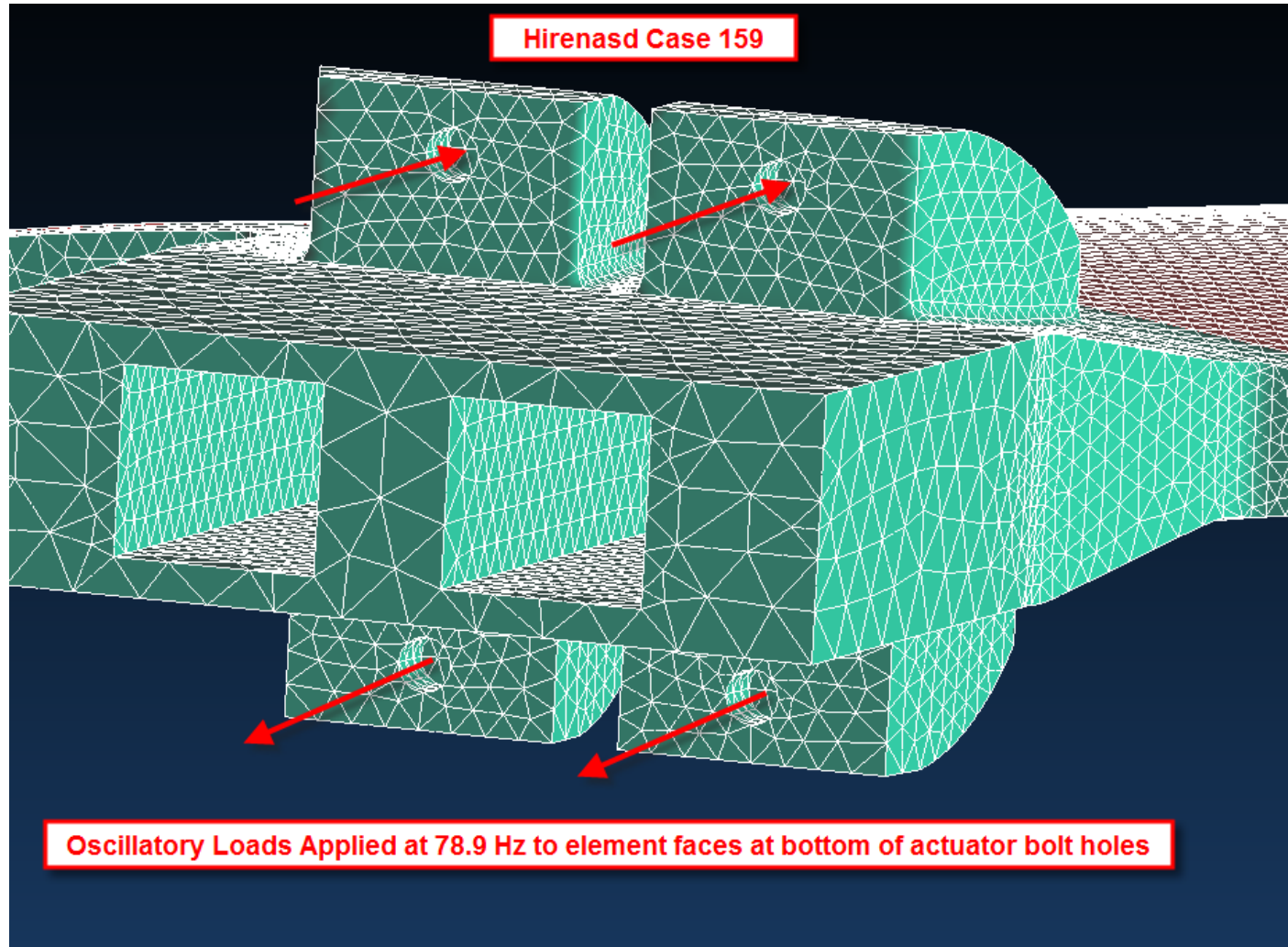
TRIA6 element face topologies on wetted elements

| | | | | | | | | |
|---------|---------|--------|--------|--------|--------|--------|--|---|
| \$! | | | | | | | | |
| WETELMG | 6047539 | TRIA6 | 347719 | 291761 | 291762 | 347762 | | + |
| + | 347720 | 285770 | | | | | | |
| WETELMG | 6047540 | TRIA6 | | | | | | + |
| + | 318165 | 318184 | 350517 | 323786 | 323784 | 323744 | | |
| WETELMG | 6047541 | TRIA6 | | | | | | + |
| + | 273334 | 273535 | 273517 | 276408 | 276411 | 276307 | | |
| WETELMG | 6047542 | TRIA6 | | | | | | + |
| + | 350517 | 285005 | 350518 | 289430 | 289428 | 350589 | | |
| ETC... | | | | | | | | |

ENDDATA

Oscillatory Load Setup

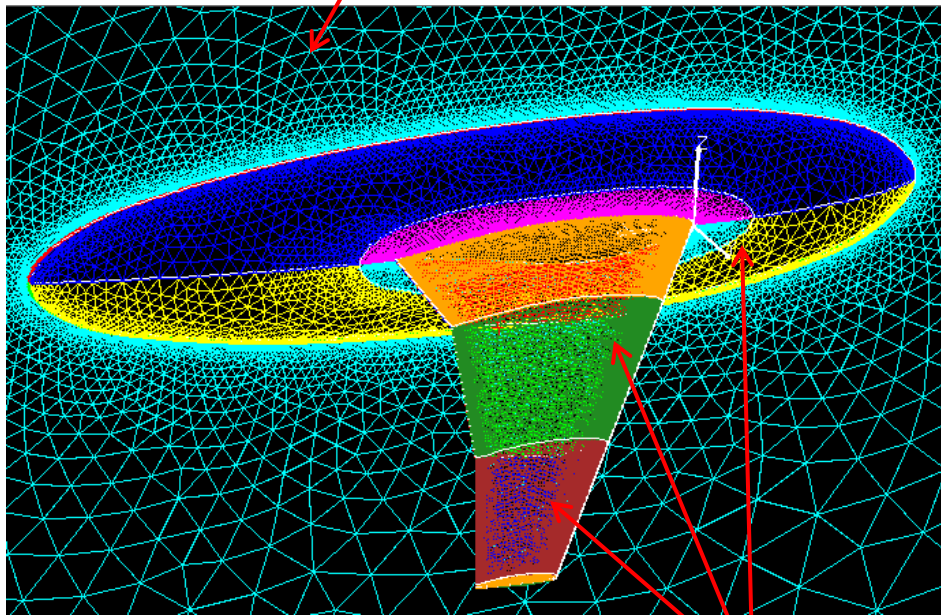
Case 159: Oscillatory Loads Scaled to obtain $\sim 2.4\text{mm}$
vacuum steady state amplitude at node 600001



CFD++ Setup

- RANS
- Turbulence model:
 - 2 equation realizable k- ϵ
 - Solve to wall for all grids
- Fluid: Nitrogen
- Steady case: coupled every 100 CFD steps
- Transient case
 - $dt = 1.268e-4$ sec (~ 100 steps/cycle)
 - 15 sub-iterations
 - Explicit FSI coupling

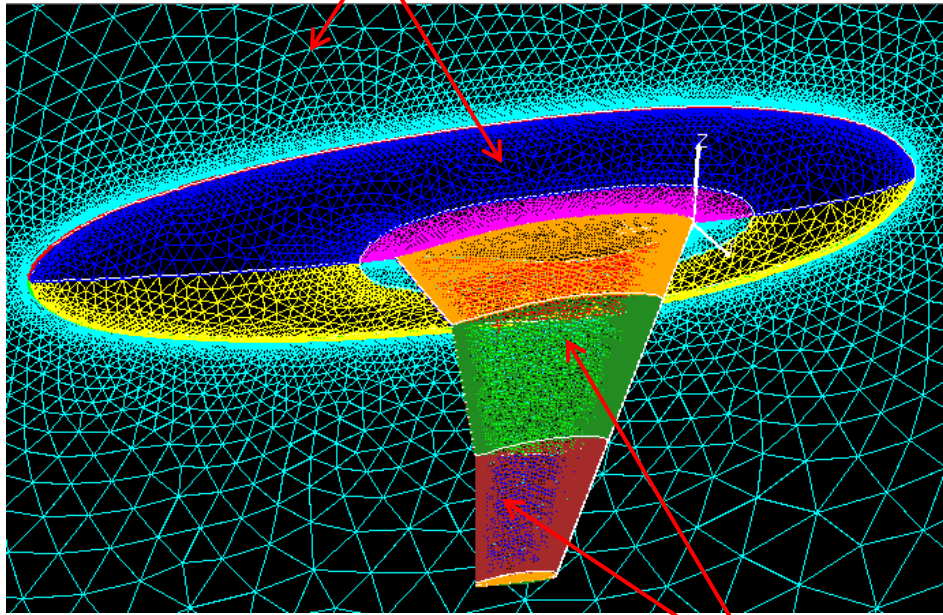
Symmetry Plane



Viscous Walls

CFD++ Setup (Morphing)

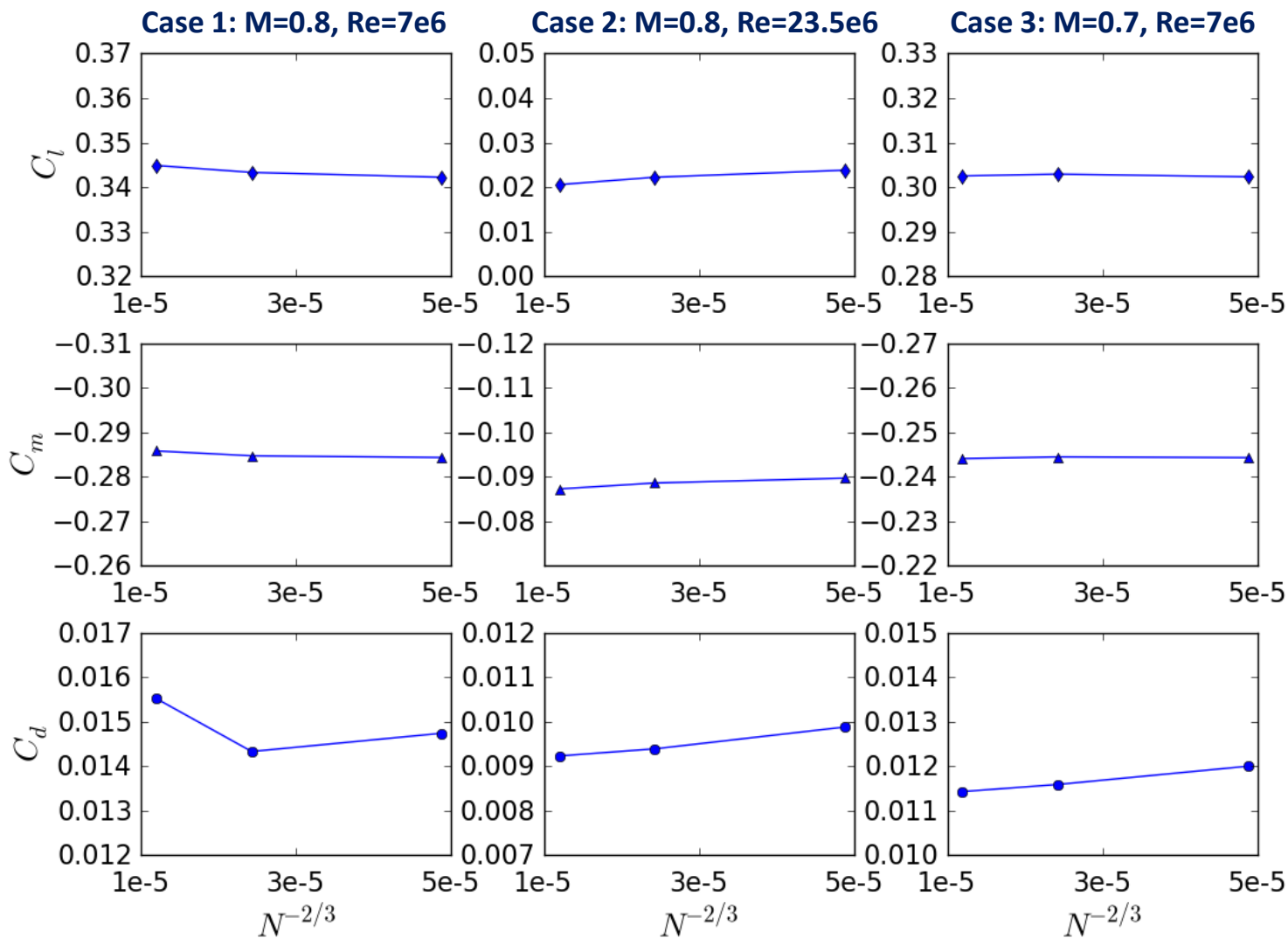
Fixed Boundaries



Moving Boundaries

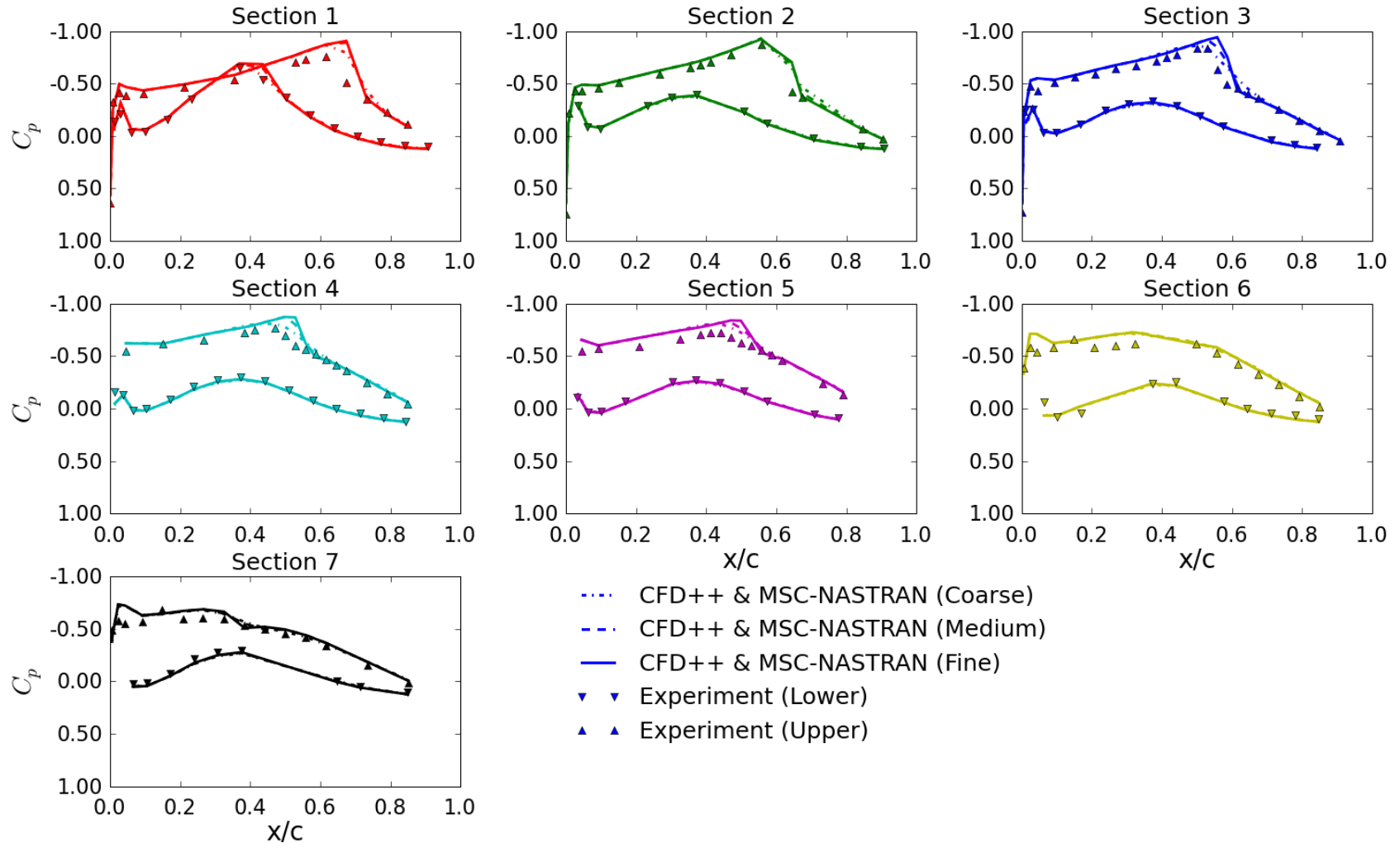
- Wing – moving
- Fuselage, Symmetry – Fixed
- Morphing restricted to a box around the wing/fuselage combination.

Grid Convergence



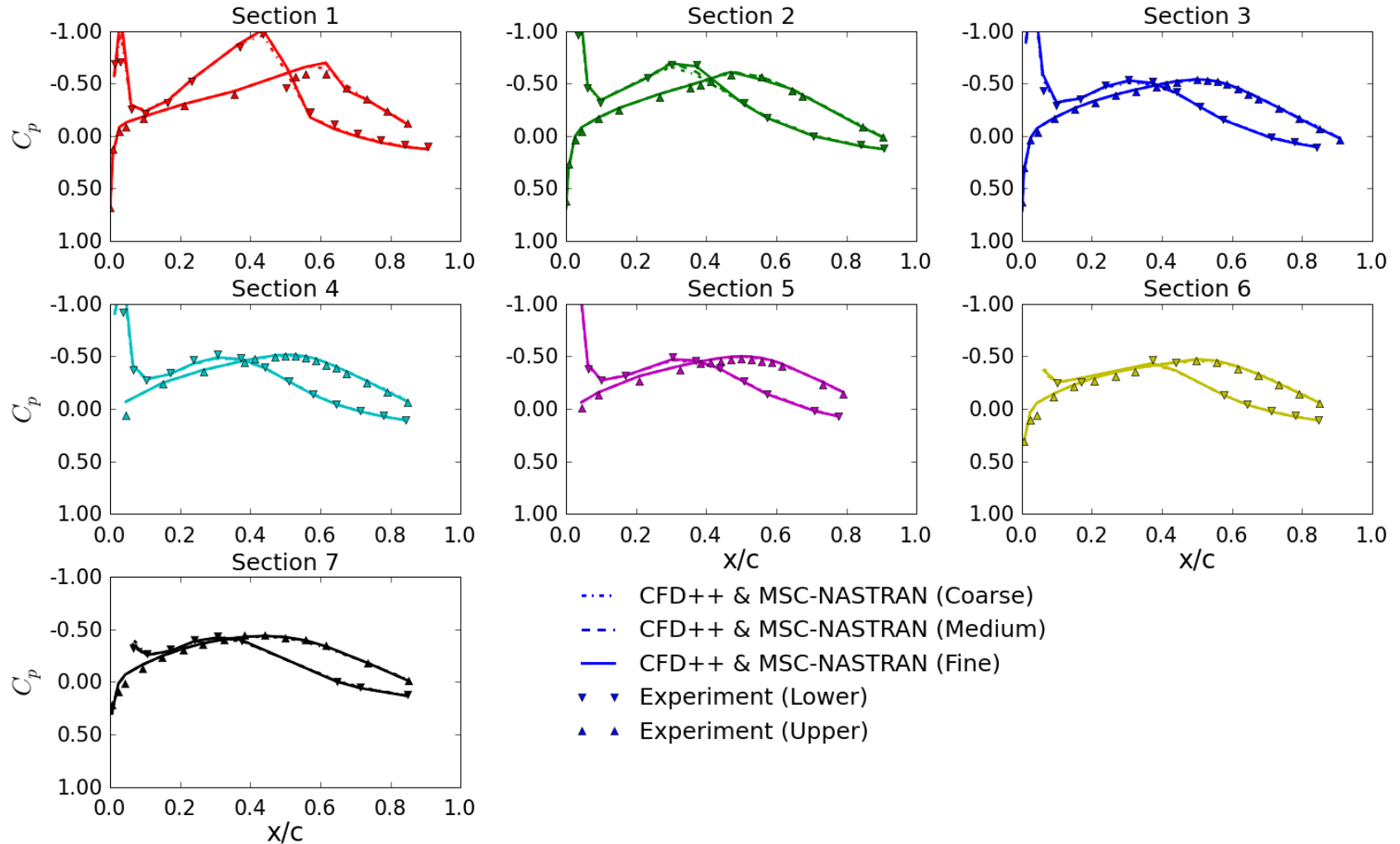
Steady State: Case1

C_p Comparison $M=0.8$, $Re = 7 \times 10^6$, $\alpha = 1.5^\circ$



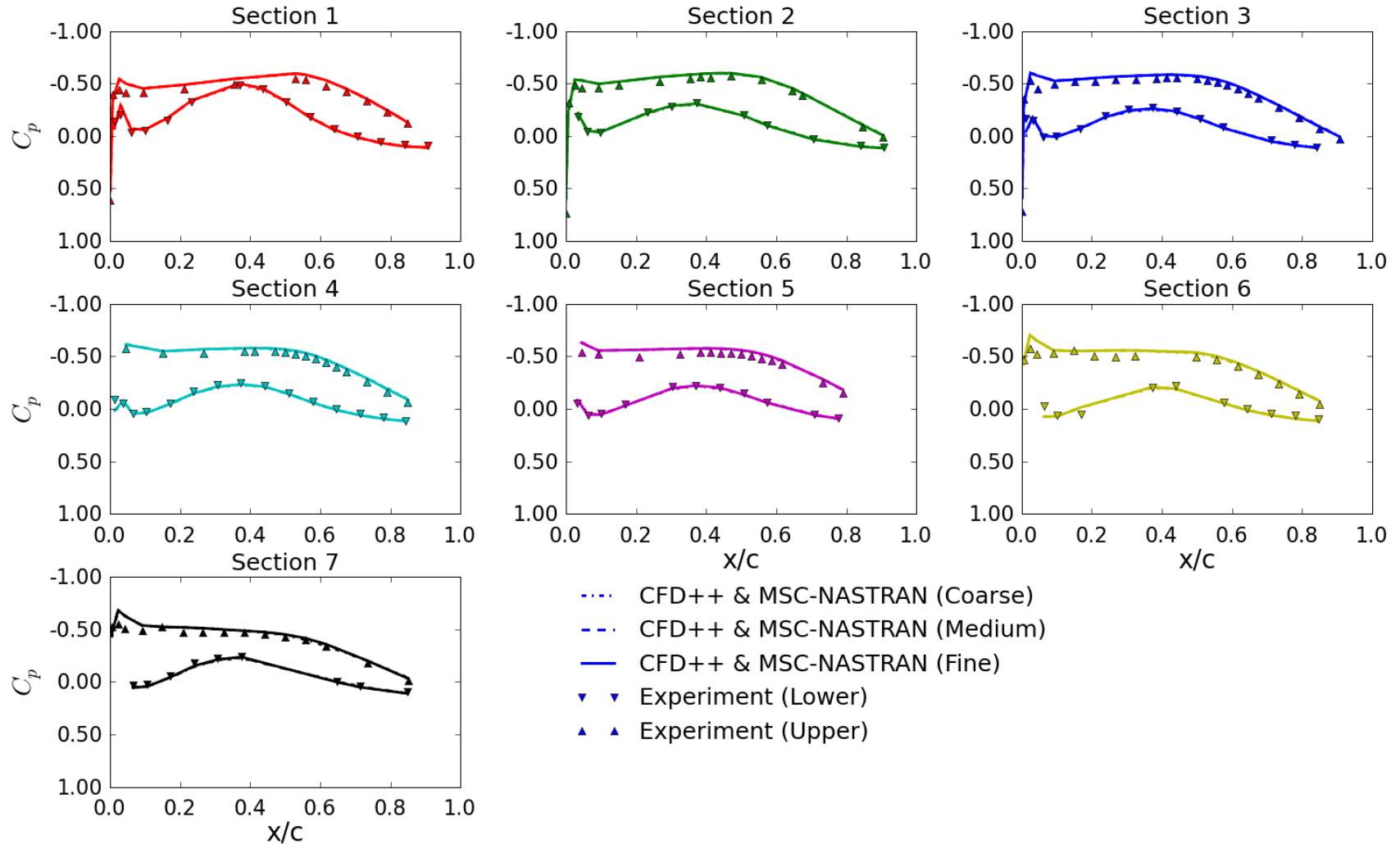
Steady State: Case 2

C_p Comparison $M=0.8$, $Re = 23.5 \times 10^6$, $\alpha = -1.34^\circ$



Steady State: Case 3

C_p Comparison $M=0.7$, $Re = 7 \times 10^6$, $\alpha = 1.5^\circ$

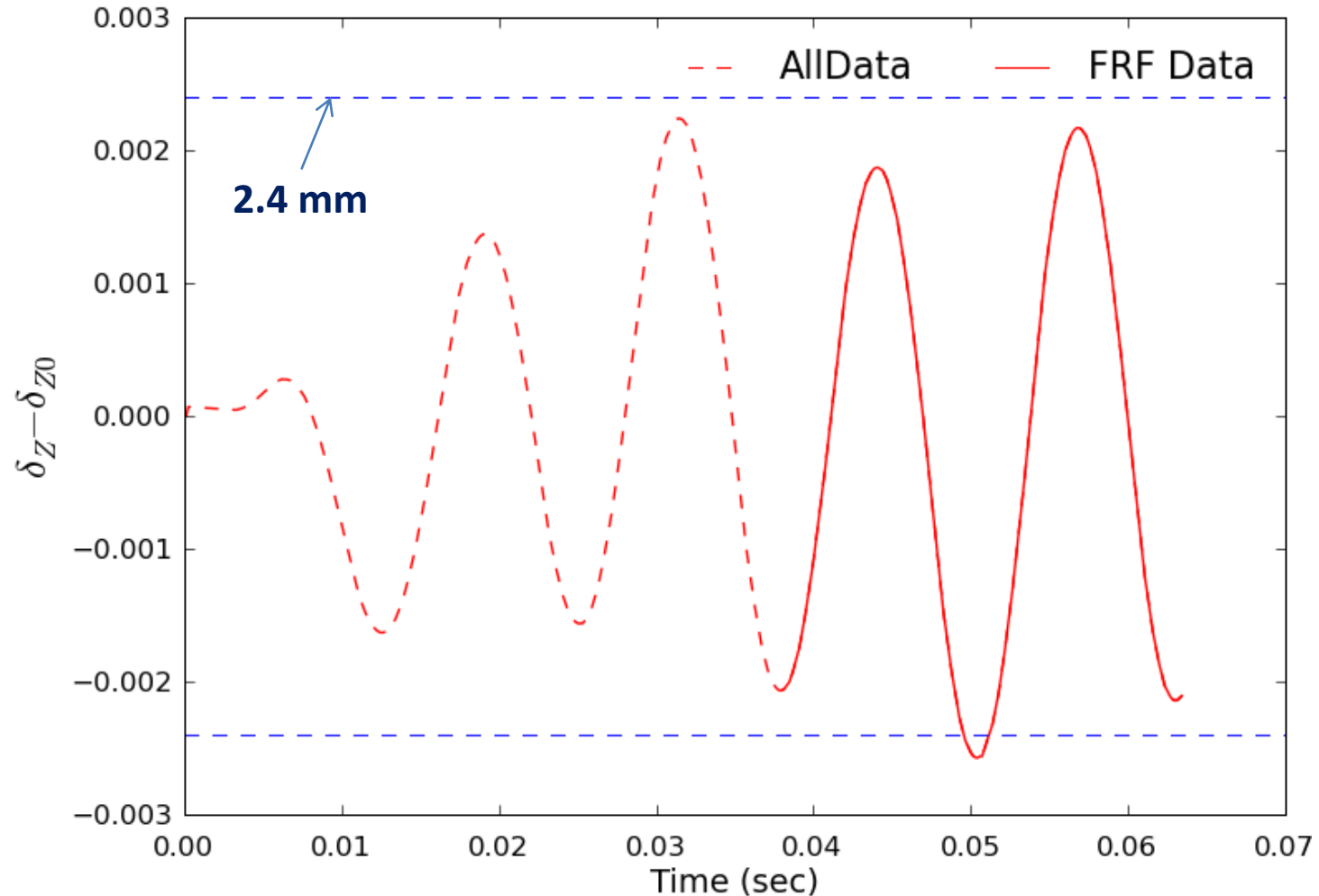


Transient Results

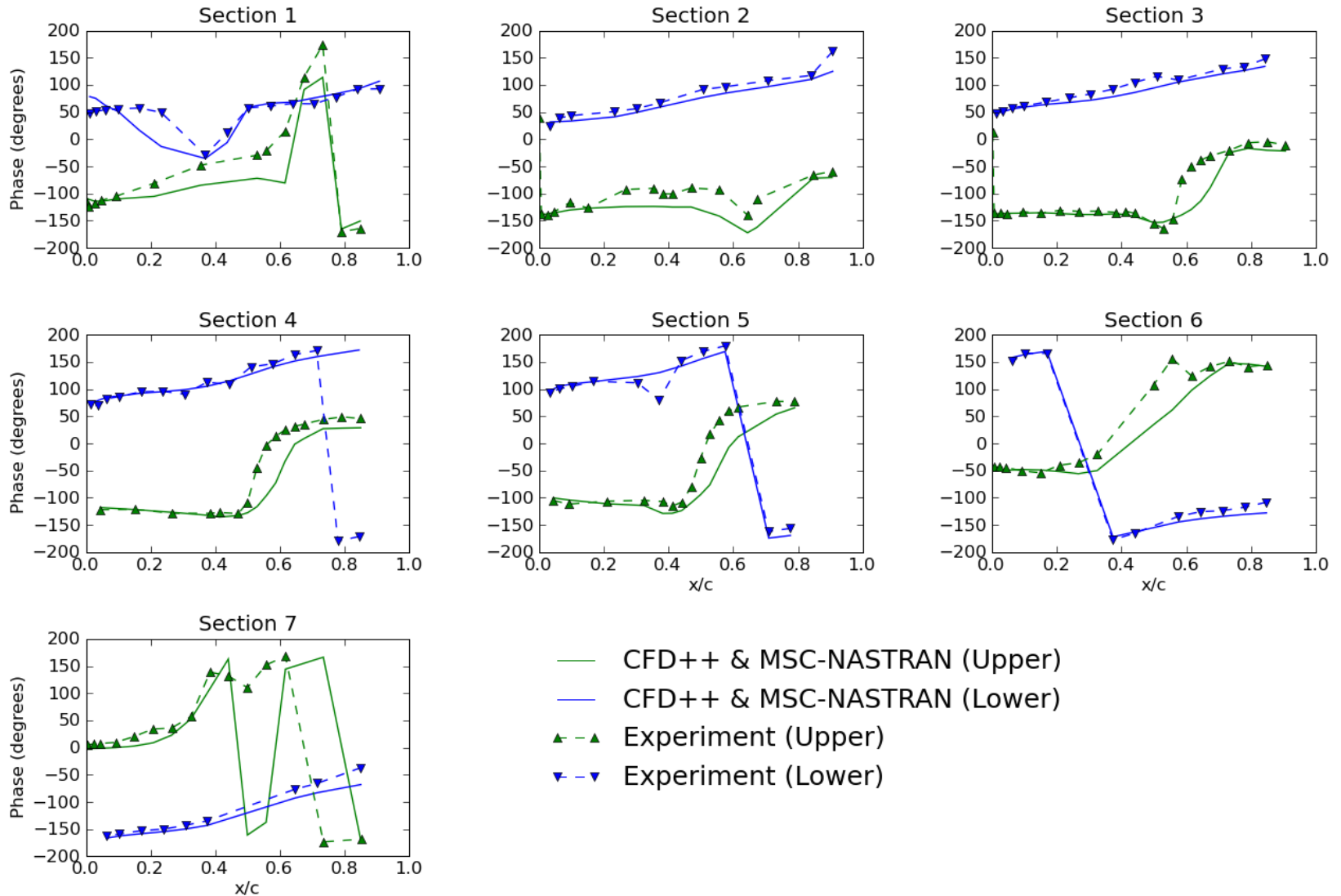
- **Transient: Plots of Cp phase and magnitude w.r.t the displacement at Accelerometer 15**
 - Oscillatory mechanical loads excite the wing
 - For the coupled analysis we had difficulty in determining the mechanical load amplitude to get the exact displacement amplitude seen in the experiment
 - This is also complicated by the fact that the excitation was at the second mode frequency (resonance)
 - Time to reach steady state was too large to allow fully coupled simulation. 20% structural damping added. (we had limited time access to the compute cluster)

Unsteady: Case 1 (Coarse)

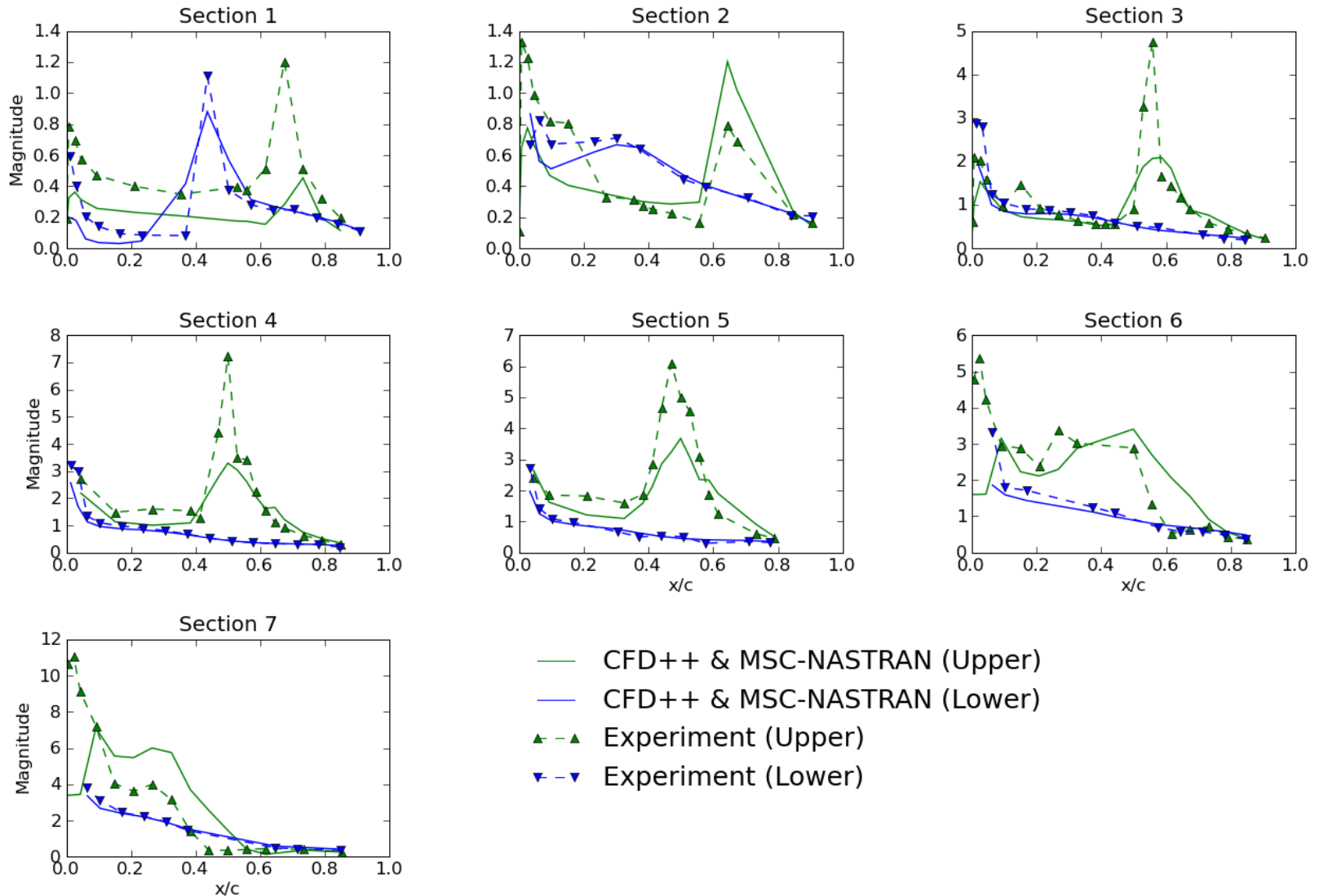
Displacement at Accelerometer 15 Location ($\delta_Z - \delta_{Z0}$)



Transient Cp Phase: Mach=0.8, Re=7e6, $\alpha=1.5^\circ$



Transient Cp Mag.: Mach=0.8, Re=7e6, $\alpha=1.5^\circ$



Hardware and Run Times

- **CFD++: 2.1 GHz AMD Opteron cluster with 24 CPUs and 128 GB per node.**
- **NASTRAN: 3.4 GHz Intel i7 CPU with 64 bit Windows and 16 GB RAM.**

| | Coarse | Medium | Fine | Coarse (unsteady) |
|--|-----------|------------|-------------|----------------------|
| No. of processors CFD/Morphing | 96/48 | 240/48 | 240/48 | 192/48 |
| Single step time (s) CFD/Morphing/ MSC-NASTRAN | 9 /60/90* | 24/415/90* | 75/2600/90* | 40/60/90* |
| Steady Run Time (hrs) 5 coupling steps | 1.46 | 4.0 | 14.15 | --- |
| Unsteady Run Time (hrs) 500 steps | | | | 26.4 |

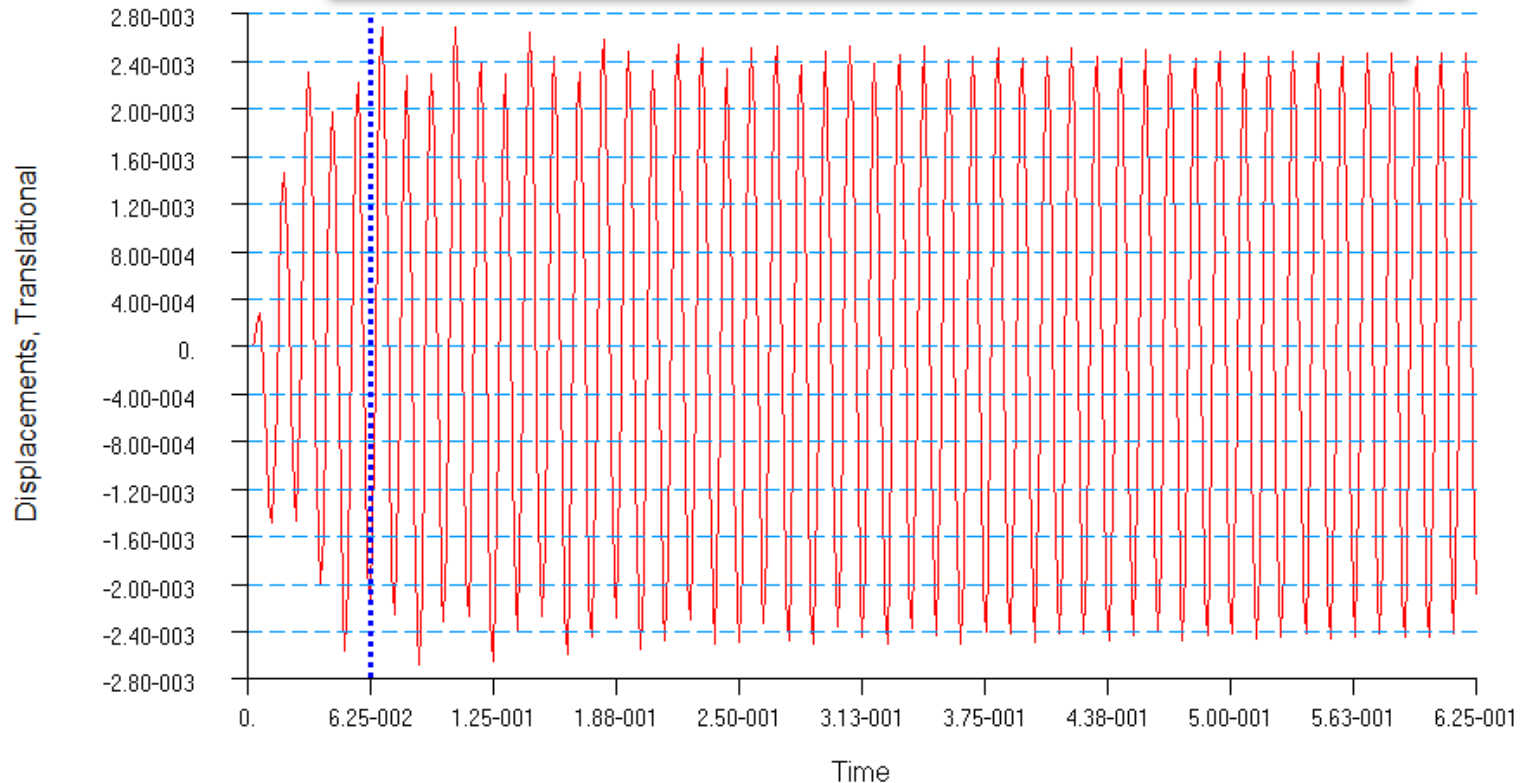
*Some uncertainty on the Nastran step time

Results Discussion

- **General coupling approach with full CFD++ and MSC-NASTRAN models**
- **Good comparison with experimental data for all steady cases**
- **Case 1: shock-like structure at inboard sections not present in experimental data**
- **Transient case:**
 - **Phase trends ok but shifted a bit aft for upper surface**
 - **Upper surface magnitudes do not match as well**
 - **Influence of mode 1**
 - **Not at steady state oscillation**
 - **Too much structural damping**

Lessons Learned/Next Steps

Node 60001 Vacuum TZ Displacement Response (20% Damping)



Would have preferred to run the coupled analysis much longer to get improved steady state results

Lessons Learned/Next Steps

- **Transient run times extensive because of time required to reach steady state**
 - **Run MSC-NASTRAN stand-alone until steady state**
 - **Use zero-crossing displacement and velocity as initial condition before starting coupled run**
 - **Reduce structural damping to more reasonable levels**

Thank You

- **Beerinder Singh**
 - 818-735-4880, ext. 259
 - bsingh@metacomptech.com

- **Jack Castro**
 - 425-891-3177
 - jack.castro@mscsoftware.com